

Neuro-Developmental Engineering: towards early diagnosis of neuro-developmental disorders

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1. Introduction

Neuro-Developmental Engineering (NDE) is a new and emerging interdisciplinary research area at the intersection of developmental neuroscience and bioengineering aiming at providing new methods and tools for: *i*) understanding neuro-biological mechanisms of human brain development; *ii*) quantitative analysis and modeling of human behavior during neuro-development; *iii*) assessment of neuro-developmental milestones achieved by humans from birth onwards.

Main application fields of NDE are:

- New clinical protocols and standards for early diagnosis, functional evaluation and therapeutic treatments of neuro-developmental disorders;
- New generations of educational, interactive toys which can provide adequate stimuli and guidance for supporting the physiological neuro-development process

This technology is expected to be also useful in the long term for developing new tools, e.g. toys, which can sustain, in *ecological* scenarios, the regular development of motor and cognitive abilities of the child, based on a rigorous scientific approach.

The long term goal is establishing standards against which development of infants at risk for neuro-developmental disorders, particularly autism, can be measured, with the aim of detecting early signs of disturbed development.

1.1 Sensori-Motor Integration Deficits in Neurodevelopmental Disorders

Neurodevelopmental disorders such as ASD, ADHD, Tourette syndrome and others are characterized by a genetic basis. In this case behavioral analysis, or behavioral phenotyping, will be instrumental for the analysis of the roles of genes in behavior (Gerlai 2002).

Autism is a behavioral disorder, with onset in childhood, which is characterized by deficits in three basic domains: social interaction, language and communication, and pattern of interests. There is no doubt that autism has a strong genetic component, and that biological disease mechanisms leading to autism are already active during foetal development and/or infancy,

as demonstrated, for example, by the abnormal pattern of brain growth during late foetal and early postnatal life (see (Keller and Persico 2003), for a review). Autism is usually diagnosed at the age of 3 years, in many cases after a period of seemingly normal neurological and behavioral development. The diagnosis of autism is purely clinical, there are no laboratory tests to confirm or disprove the diagnosis. It has been recognized that, although typical autism is not associated with major neurological deficits, autism has characteristic manifestations in the *perceptual and motor domains*.

Deficits in the *perceptual domain* include altered processing and recognition of socially relevant information from people's faces (see (Grelotti et al. 2003), for a review), deficits in perception of motion cues (Milne et al. 2002), (Spencer et al. 2000), (Bertone et al. 2003), (Takerae et al. 2004), difficulty in disengaging attention (Landry and Bryson 2004) and alterations of auditory processing (Courchesne et al. 1984), (Boddaert et al. 2004). Studies based on analysis of home-made movies suggest that an impairment of spontaneous attention toward social stimuli is present already at 20 months (Swettenham et al. 1998), and possibly also as early as during the first 6 months of life (Maestro et al. 2002). Furthermore, an autism-like syndrome is frequently observed in congenitally blind children (Hobson and Bishop 2003). Taken together, these observations suggest that at least some individuals with autism are characterized by an early deficit of 'low-level' perceptual processing, which jeopardizes their ability to develop higher-level capacities, such as language and interpersonal skills.

Motor impairments in autism include deficits in postural reflexes (Minschew et al. 2004), (Schmitz et al. 2003), (Molloy et al. 2003), repetitive, stereotyped movements and awkward patterns of object manipulation, lack of purposeful exploratory movements (see e.g. (Pierce and Courchesne 2001)), gaze abnormalities (Sweeney et al. 2004), unusual gait pattern (Hallett et al. 1993), and alterations of movement planning and execution, which express themselves as 'hyper-dexterity' (Rinehart et al. 2001), (Mari et al. 2003). Motor abnormalities may be observed retrospectively in infants who later develop the autistic syndrome, on the basis of home-made movies made during the first year of life (Teitelbaum et al. 1998), (Teitelbaum et al. 2004). These clinical observations are consistent with a large body of evidence of subtle structural and functional abnormalities of cortical and subcortical neural systems involved in *movement planning and execution*, such as the prefrontal cortex, the basal ganglia and the cerebellum (see (Keller and Persico 2003), for a review).

1.2 Ecological Approach

The diagnosis of ASD is currently made at 3 years of age; Attention-Deficit Hyperactivity Disorder (ADHD) is always considered as an alternative diagnosis of "high functioning" autism; Tourette syndrome is diagnosed at age 7 or later. ASD is therefore a natural candidate for demonstrating the validity of novel approaches to early diagnosis. As shown in Fig. 1, infancy, i.e. the first 2-3 years of life before language development, represents an important temporal window for an early diagnosis of ASD.

The goal of our approach is twofold. On one hand, guided by neuroscientists, we develop technological platforms and methods to extract more information on perceptual and intersubjective capacities of human infants than is currently possible; this information could be later used for early diagnosis of developmental disorders. On the other hand, infancy provides us with an important window of opportunity to capture the mechanisms behind sensorimotor integration as these are just developing. Moreover, neurodevelopmental disorders are an important benchmark to highlight failures within such mechanism. Such a knowledge can be useful to neuroscientists to better understand the human brain functions involved in the

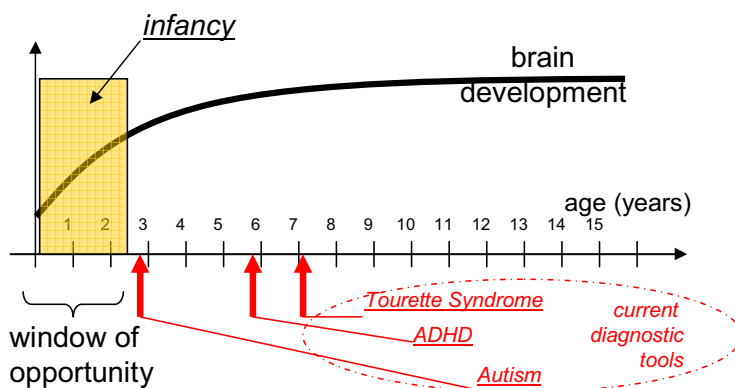


Fig. 1. Current diagnostic tools

sensorimotor integration but also to engineers, providing unique insights on how to build complex and adaptable artificial systems (Metta et al. 1999).

2. Technology for Assessing Movement and Gaze

2.1 Motion Tracking

Motion tracking can count on a host of different technological solutions, operating on entirely different physical principles, with different performance characteristics and designed for different purposes. As shown in (Welch and Foxlin 2002), there is not a single technology that can fit all needs. Each application defines the best technology to be implemented. In order to perform a selection, the main characteristics of available technologies are briefly summarized hereafter (see (Welch and Foxlin 2002) for details).

Mechanical sensing:

typically used for body motion capture; it uses angle and range measurements with the help of gears and bend sensors; very accurate but *bulky*, often limiting mobility.

Optical sensing:

several principles are available, typical systems are camera-based ones; position of markers in 3D space can be estimated very accurately within working volume (typically a few cube meters, depending on the number of deployed cameras); line-of-sight issues (i.e. the fact that body parts or other objects may occlude the visual scene of a camera, losing thus the sight of one or more markers) is a limiting factor; very expensive; often requires highly structured environments, at least when high accuracy is needed.

Acoustic sensing:

typically based on time-of-flight of ultrasound pulses between emitters and receivers; sound speed in air (about 340 m/s , resulting in sampling periods in the order of a few tens of milliseconds) is slow but still acceptable for sensing human (in particular infants) movements; line-of-sight issues are not as severe as for the optical technology; requires much less structured environments than optical trackers; suitable to be used in ecological conditions (e.g. kindergartens).

(Geo)Magnetic sensing:

a first method is based on electromagnetic coupling between a source and several trackers; main drawbacks are that signal decays as $1/d^3$ (where d is the source-tracker distance) and is affected by the geomagnetic field; these devices are quite expensive and require a certain amount of structuring of the environment. A second method is electronic compassing; estimates heading and solely relies on the *geomagnetic* field, i.e. it does not require any artificial source and is therefore *sourceless*; measurements can be altered by ferromagnetic influence of surrounding objects.

Inertial sensing:

highly miniaturized accelerometers and gyroscopes are used to sense, respectively, acceleration (comprising the gravitational field) and angular velocity; used as inclinometers, accelerometers can sense the gravity vector, i.e. the 'vertical' direction, in this sense they are also *sourceless*.

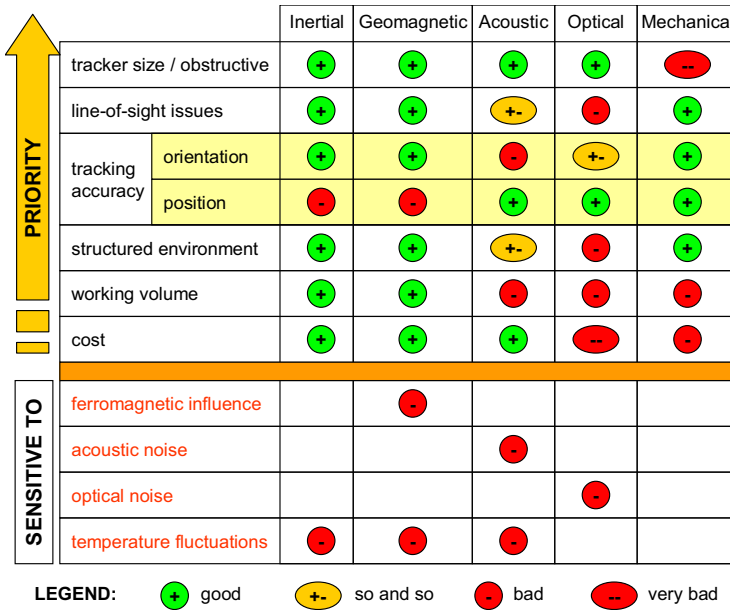


Fig. 2. Selection chart of different motion tracking technologies

In Fig. 2, a selection chart for the different available technologies is provided. For each available technology (columns) its suitability with respect to the performance characteristics of interest (rows) is indicated. Since our main purpose is developing technological tools that are either wearable by infants or embeddable into toys, the highest priority is given to technologies which are unobtrusive. This directly leads us to discard solutions involving mechanical trackers.

The second element considered for selection are the line-of-sight issues, since we are going to deal with infants, it is extremely difficult to perform experiments with technologies that are limited by the line of sight, a peculiarity of the optical technology which is only suitable to

experiments with collaborative subjects who are somehow willing to 'act' in front of a camera. Line-of-sight issues are much less severe for the acoustic technology which is thus still appealing for movements analysis in infants.

The third element of the selection criterion is performance with respect to tracking accuracy. Here a distinction is made between tracking positions and tracking orientations. Measurement principles such as the time-of-flight (typically deployed in acoustic measurements) or camera-based tracking are inherently suitable to measure the distance of points (markers) and the origin of the measurement system (e.g. the source of acoustic waves or a camera etc...). Orientations can be inferred indirectly by estimating distances between two or more markers and the source of measurement. The larger the distance between two markers, the better the estimation of orientation. As dimensions shrink, as in the case of infants, accuracy of indirect orientation measurements also decreases (e.g. accurate tracking of the orientation of an infant's wrist can be problematic even without considering line-of-sight issues). Other technologies allow a direct measurement of orientations (for example inertial sensors used as inclinometers can sense deviations from the vertical axis while magnetic sensors used as compasses can sense deviations from the horizontal geomagnetic north direction) without requiring the positioning of multiple markers.

As long as orientation is concerned, inertial and magnetic technologies appear to be very appealing since: are highly unobtrusive due the availability of miniaturized off-the-shelf devices; do not suffer from line-of-sight issues; can provide high accuracy in orientation tracking are *sourceless*: do not require any structuring of the environment; have virtually unlimited working volume; are low-cost.

The bottom half of Fig. 2 shows, for each technology, the main limiting factors to a correct operation. Besides temperature, which affects any electrical device and that can be compensated in most of the cases, the real limiting factor for the magnetic technology is the presence of ferromagnetic materials. Common ferromagnetic objects such as iron parts of doors, chairs, tables etc... can produce local distortions of the geomagnetic field, causing thus errors in the estimations of orientations. As discussed in (Kemp et al. 1998), some care should be taken, when conducting experiments, to avoid large ferromagnetic objects in the surroundings. We found that this can be easily done in environments such as day-cares where, for safety reasons, all metals are usually avoided and typical materials used with children are wood, rubber and plastic.

2.2 Gaze Tracking

Devices for measuring eye movements are commonly referred to as 'eye trackers'. In general there are two types of techniques for monitoring eye movement (Young and Sheena 1975):

- 'eye-in-head' measurement: the sensing device is fixed on the head and therefore the eye position is measured in craniotopic coordinates;
- 'point of regard' or gaze: the sensors are located in the external environment and the eye position is measured in spatial coordinates.

These two kind of measurements are coincident when the head is kept in a fixed position. When the head is free to move, measurement of the head orientation is also required to derive gaze from craniotopic coordinates. Eye tracking methodologies can be classified in four categories:

1. Magnetic Induction Method (Search Coil)
2. Electro-Oculography (EOG)

3. Photoelectric Methods: Infra-Red (IR) Oculography
4. Video-Oculography (VOG)

Each methodology is characterized by parameters such as range of measurement, sensitivity, linearity, accuracy, discomfort for the subject, interference with the field of view of the subject, tolerance to head movement.

Magnetic Induction Method (Search Coil):

The search coil technique has become the accepted standard for the measurement of 3D eye movement. This technique is based on the fact that a magnetic field induces a voltage in a coil (search coil) which is attached to the eye. The induced voltage has amplitude proportional to the sine of the angle between the coil axis and the magnetic field direction. The magnetic field is provided by coils mounted at the sides of a cubic frame. The dimensions of the sides of the frame can vary from few tens of centimeters to few meters, allowing to measure also other movements (i.e. eye-hand coordination). Robinson (Robinson 1963) was the first to apply this technique, using a coil secured to the eye by suction. Nowadays the search coil is embedded in a scleral contact lens. The lens is subject to slippage if the lens covers only the cornea. Eye movement is measured in absolute spatial coordinates. Head orientation can also be measured with a search coil mounted on the forehead, and orientation and movement of the eye within the head can be calculated from the orientation of the head and of the eye with respect to the magnetic field (Haslwanter 1995). Currently a number of different search coil systems are commercially available (e.g. by Skalar Instruments, C-N-C Engineering, Remmel Labs, etc.). Although the scleral search coil is the most precise eye movement measurement method (very high temporal and spatial resolution can be obtained with accuracy to about 5-10 arc-seconds over a limited range of about 5 deg), it is also the most intrusive method. Insertion of the lens requires care and practice and wearing the lens causes discomfort and risk of corneal abrasion or lead breakage. The requirements to stay in the center of the magnetic field precludes the use of search coils during many natural activities. Thus, this technique is mostly used for research purposes, it is not suitable for clinical routine.

Electro-Oculography:

First applications of electro-oculography are dated back to the '30s and are currently widely used both for clinical and research purposes. It relies on measurement of electrical potential differences between the cornea and the retina, discovered by DuBois-Reymond in 1849. Skin electrodes are positioned around the eye. The measured potential difference is proportional to the sine of the rotation angle of the eye. For small rotation the proportionality is almost linear; it decreases for higher angles of rotation (Byford 1963). The recorded potentials are in the range 15-200 μV , with nominal sensitivities of order of 20 $\mu\text{V}/\text{deg}$ of eye movement. The eye movement is measured in craniotopic coordinates and head movement during recording does not affect the measurement. The discomfort for the subject is limited and the measurement range is wide both for horizontal movements (± 70 deg) and for vertical movements (± 30 deg), even if the sensitivity decreases for lateral position of the eye. The most important advantage of this methodology is the possibility of recording eye movement with closed eyes, which is relevant requirement during some experimental protocol (e.g.. during sleeping phases). The main drawback of this technique are related to the nature of the potential recorded and to the artifacts due to the electrodes properties. As concern the potential, the resting corneo-retinal potential (usually of the order of 0.4-1 mV) can be affected by lighting conditions of the environment and by the psycho-physical condition of the subject. The artifacts at the

level of the skin electrodes relies on the contact resistance electrode-skin, on the oxidation and polarization of the electrodes.

Infra-Red Oculography:

Infra-red (IR) oculography is based on the recording of the light reflected by the eye when it is lighted with IR light beam. Since IR light is not visible, it does not interfere with the subject vision, moreover the IR detectors are not influenced by environmental lighting conditions. There are three categories of Infra-red (IR) oculography which use respectively: the corneal reflection, the Purkinje images and the track of the limb. Due to the construction of the eye, when a beam of IR light points to it, four reflections are formed on the eye, called Purkinje images (Cornsweet and Crane 1973): the first on the front surface of the cornea and it is called corneal reflection, the second image on rear surface of the cornea, the third on the front surface of the lens and the fourth on the rear surface of the lens. By detecting the corneal reflection and the pupil center and by using an appropriate calibration procedure, it is possible to measure the Point of Regard (gaze) on a planar surface on which calibration points are positioned. Two points of reference on the eye are needed to separate eye movements from head movements. The positional difference between the pupil center and corneal reflection changes with pure eye rotation, but remains relatively constant with minor head movements. The corneal reflection moves in the opposite direction of the eye respect to the pupil center. In other cases both the first and the fourth Purkinje images (Dual-Purkinje images eye trackers are detected. Both reflections move together through exactly the same distance upon eye translation but they move through different distances upon eye rotation. The third method based on photoelectric principle relies on the track of the limb (scleral-iris edge) of the eye by measuring the amount of scattered light. Most photoelectric systems must be mounted close to the eyes (i.e. EL-MAR tracking device), so they may restrict the field of view, moreover fast movements of the head can cause slippage of the device on the head leading to mis-alignment of the eye respect to the IR emitter and detector. There exist also external device and a support for keeping the head fixed is needed (i.e. Tobii eye tracker). The range of measurement of the photoelectric eye tracker is not higher than ± 30 deg in the horizontal plane and ± 20 deg in the vertical plane.

Video-Oculography:

Video systems for measuring ocular movements are based on the analysis of images recorded by cameras. This technique, introduced in the '80s, quickly improved in terms of performances and reliability thanks to the technological development of digital cameras and computer powerful. The Video Oculography (VOG) provides directly a digital output. Several algorithms are available for the pupil detection in an image frame and pupil centroid coordinates extraction, nevertheless environmental lighting conditions can affect the automatic detection (Eizenman et al. 1984) (Landau 1987). Thus, IR light is used together with video recording, so that the pupil appears brighter. This technique is called Pupil Center/Corneal Reflection (PC/CR) because the IR light produces also the Purkinje images, mentioned before. As in IR Oculography, also VOG can be realized both as wearable device (DiScenna 1995) and provides measurements in craniotopic coordinates or external device and provides measurements in spatial coordinates. Head-mounted system (i.e. EyeLink) can be worn without too much discomfort. High resolution and high frame rate CCD and CMOS cameras are used. Reduced dimensions and weight of the actual cameras allow to position them in such a way that they interfere as less as possible with the field of view of the subject (Babcock and Pelz

2004), (Pelz et al. 2000). The measurement range for VOG systems can exceed ± 30 deg in horizontal plane and ± 20 deg in the vertical plane; eye tracking can be executed both on-line and off-line. The drawback is that these systems have a low acquisition rate, in general 50-60 Hz, not suitable for recording fast eye movement such as saccadic movements, but suffices for smooth pursuit eye movements. External camera systems can go up to 1000-1250 Hz and have an accuracy of 0.01 deg. External camera are generally positioned under the screen of a computer, used for calibration and for specific visual stimuli. Head movements are tolerated if the eye is kept in the field of view of the camera. There are devices which include systems of pursuit of the subject and the camera orients automatically so that the eye of the subject is always in its field of view.

In Table 1 the relevant parameters of the eye tracking techniques presented are summarized.

3. Instrumented Toys and Wearable Devices

Virtually any toy, tool or piece of garment used by children could be a good candidate to host all sorts of technology and 'see what comes out' when the child wears it or plays with it.

Our approach is based on a closed-loop dialogue between neuroscientists and bioengineers. In the following, two platforms are presented which specifically address two domains of interest in child's development: spatial cognition and social behavior.

For both platforms, functional specifications are derived from protocols of experiments of interest for neuroscientists. The aim is twofold. On one side we wish to provide neuroscientists with novel technological platforms for the unobtrusive and ecological assessment of behavioral development in infants. On the other side, these platforms should enable/facilitate the transition from research to clinical practice.

3.1 Assessing Spatial Cognition Skills

By the end of the first year of life, infants start to pile-up blocks, put lids on cans and insert objects into apertures. Through these activities, the child learns to plan actions that involve more than one item. The ability to solve such problems reflects the child's spatial, perceptual and motor development. In particular, the representational ability to imagine objects in different positions and orientations must be in place before various objects can be fit into apertures.

Recent studies by Ornkloo and von Hofsten (Ornkloo and von Hofsten 2007) show developmental curves, based on statistical rates of success of object-fitting tasks, relative to children aged 14-26 months old.

Specifically, the tasks consisted of inserting cylinders with different cross-sections into a box with similar holes on its lid, see Fig. 3 (top). All the objects had similar dimensions, 1 mm smaller than the apertures. Different cross-sections were used whose circumference was approximately the same but varied with respect to the number of possibilities they fit into a corresponding aperture, as also reported in Fig. 3 (bottom).

Based on visual inspection of video recordings, the data analysis consisted (among other things) in assessing horizontal and vertical pre-adjustments. In particular, the outcome was yes/no (i.e. successful or unsuccessful) based on the alignment errors between the object and the box. Both the vertical error (angular misalignment between the longitudinal axis of the object and verticality) and the horizontal error (angular misalignment between the orientations of the cross-section and the aperture) were estimated (from the videos). Results showed that successful solution was associated with appropriate preadjustments before the hand arrived with the block to the aperture; in particular it has been proved that the preadjustments can be considered appropriate for misalignments lower than 30 deg.

	Search coil	Electro-Oculography	Infra-Red Oculography	Video Oculography
<i>Measurement Typology</i>	Absolute spatial coordinate	Craniotopic coordinates	Head-mounted: craniotopic coordinates; External device: spatial coordinates	Head-mounted: craniotopic coordinates; External device: spatial coordinates
<i>Range of measurement</i>	±90 deg for all 3D space	±70 deg in horizontal plane ±30 deg in vertical plane	±30 deg in horizontal plane ±20 deg in vertical plane	±30 deg in horizontal plane ±20 deg in vertical plane
<i>Temporal Resolution</i>	linked to A/D conversion, 500-1000Hz (depends on software and hardware instrumentation)	linked to A/D conversion, 500-1000Hz (depends on software and hardware instrumentation)	linked to A/D conversion, 500-1000Hz (depends on software and hardware instrumentation)	Depends on camera frame rate: from 30Hz to 1000-1250Hz
<i>Spatial resolution</i>	0.01 deg	1-1.5 deg	0.1 deg	0.1 deg
<i>Discomfort</i>	High	Limited	Limited	Limited
<i>Interference with the subject field of view</i>	None	None	Head-mounted device can interfere with the field of view	Head-mounted device can interfere with the field of view
<i>Tolerance to head movement</i>	- Head has to be in the center of the magnetic field - Additional search coil on the forehead	Not affected by head movement	External device: low tolerance to head movements	- Head movements are tolerated when eye is kept in the field of view of the camera; - Additional sensors allow to re-orientate the camera
<i>Other Notes</i>	- limited recording time and risk of corneal abrasion or lead breakage - lens slippage	- Measurement with closed eyes (during sleeping) - Skin electrodes artifacts - Resting corneo-retinal potential variability	- Not suitable when the subject wears glasses or contact lens	

Table 1. Comparison of different gaze tracking technologies

3.1.1 Block-Box Platform

Inspired by such experiments and based on our previous experience with sensorized toys (Campolo et al. 2007), we developed a sensorized core, shown in Fig. 4 (top), for the cylindrical

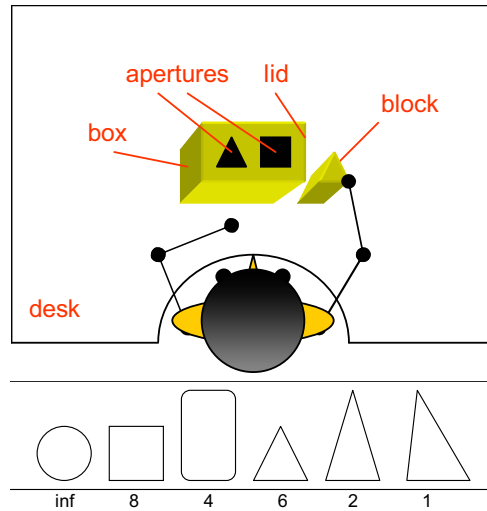


Fig. 3. Block-box experimental scenario (top). Different cross-sections (bottom) for the cylindrical blocks and the relative number of insertion possibilities ('inf' means infinite), readapted from (Ornkloo and von Hofsten 2007)

objects with various cross-sections, shown in Fig. 4 (bottom).

In particular, we found that from an *ecological* perspective, the *sourceless* estimation of objects orientation via inertial and magnetic sensors is especially suited to this application. Accelerometers can in fact be used to measure tilt while magnetometers can be used as compass to measure horizontal misalignments. Gyroscopes are required to compensate for non-static effects. Further details on the filter used to estimate orientation from the sensors raw data is described in (Campolo et al. 2008).

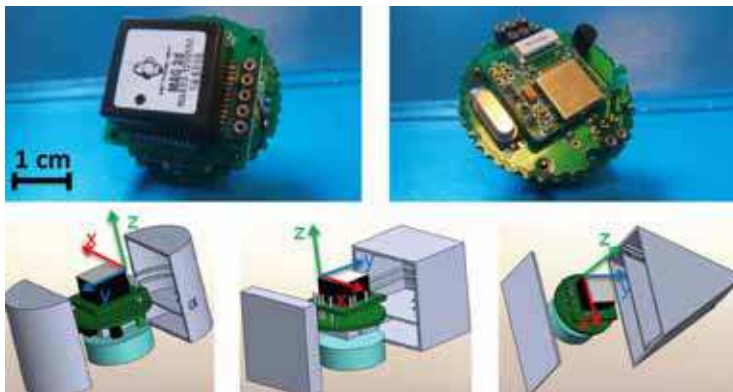


Fig. 4. Kinematics sensing unit (top left). Bluetooth transmitting unit (top right). Examples of assemblies of electronics and batteries for shells with different cross-section (bottom).

By considering the requirements of the experimental setup and protocol of the above mentioned study (Ornkloo and von Hofsten 2007), the functional specifications of the block-box platform can be resumed as follows:

- the device (electronic core and power supply) should be embeddable in solids with different shapes with a “grasping size” less than 5 cm;
- the sensor unit should consist of sourceless sensors for orientation tracking;
- the transmission unit should assure a bi-directional wireless communication to a remote workstation few meters far from the experimental scenario;
- the batteries should provide power supply for at least 2 hours of continuous use;
- the overall weight of the toy should not exceed the 50-60 grams.

According with these specifications, the block-box sensorized toys have been designed to be as compact and light as possible. In particular, the platform mainly consists of a compact (17.8mm × 17.8mm × 10.2mm), micro-fabricated 9-axis inertial-magnetic sensor (model MAG02-1200S050 from Memsense Inc.). The device is designed to sense $\pm 2g$ accelerations, ± 1200 deg/sec angular rates, ± 1 Gauss magnetic fields, all within a 50 Hz bandwidth. The sensors are coupled with a multi-channel, 12 bits AD converter (model MAX1238 from Maxim Inc.) which can retransmit converted data over a 4-wires I2C bus. For our application, we sample each of the 9 channels at 100 Samples/sec rate. Such data are collected and rearranged in a specific message format by a microcontroller (PIC16F876A from Microchip Technology Inc.) and then retransmitted via a bluetooth module (Parani-ESD200 from Sena Technologies Inc.). Finally, two 3.6V Li-Ion Rechargeable batteries (LIR3048 from Powerstream Inc.) are used in series, in order to guarantee approximately two hours of autonomous operation. Data transmitted over the bluetooth interface are collected by a nearby PC, for later data analysis. Fig. 5 represents the overall architecture of the block-box platform. As it can be noted, we decided to arrange the different components into two separate electronic boards (a sensor board and a transmission board), which are connected through the I2C bus. This solution makes the system modular, allowing us to easily change the sensor unit or put together several sensors that share the same bus.

In Fig. 6 the electronic CAD designs (left) and the real pictures (right) of the sensor (top) and the transmission (bottom) boards are shown. Fig. 7 reports the overall aspect of the electronic core of the Block-Box platform with the actual dimensions.

3.1.2 In-Field Calibration of Inertial-Magnetic Sensors

Magnetometers are meant to sense the geomagnetic field and provide its components $[b_x, b_y, b_z]^T$ along the \hat{x} , \hat{y} and \hat{z} axes of the sensing device itself (such axes move with the moving frame). Similarly, the accelerometers are meant, in static conditions, to read out the components of the gravitational field $[g_x, g_y, g_z]^T$ along the same axes.

Calibration of such sensors is straightforward when one can reliably count on precision alignment procedures, e.g. in a laboratory setting. In (Campolo et al. 2006), a procedure for in-field calibration of magnetometric sensors was presented which does not rely on previous knowledge of magnitude and direction of the geomagnetic field and which does not require accurately predefined orientation sequences. Such a method can be applied to accelerometers as well and is especially suited for clinical applications. The procedure relies on the fact the geomagnetic (or gravitational) field has constant components in the fixed frame. As the orientation of the sensors vary, the components in the moving frame also vary but the magnitude

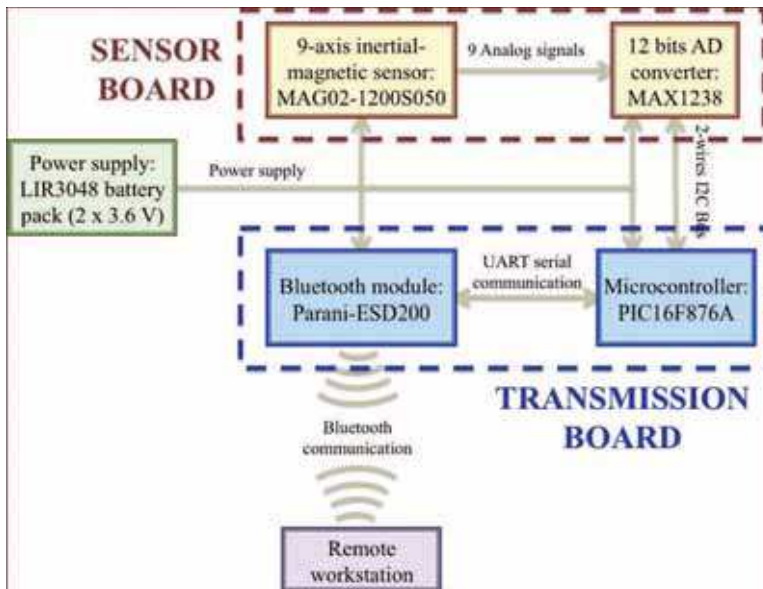


Fig. 5. Block-Box Platform architecture.

of the field keeps constant, i.e. the components are bound to lie on a sphere. Readouts from non-calibrated sensors are therefore bound to lie on an ellipsoid, see (Campolo et al. 2006) for details. Via the least-square method it is possible to robustly estimate the centroid and semi-axes length of the ellipsoid which coincide with the calibration parameters (gain and offsets for each axis).

Based on this method, a calibration protocol was devised to provide a sufficient number of measurements for the algorithm to robustly converge. The instrumented toy (of whatever shape) is secured inside a wooden box, shaped as a parallelepiped, so that the toy does not move as the box is displaced around.

Magnetometers:

as in Fig. 8-a, the box is placed on a table and an approximately 360 deg rotation (no need to be accurate) is performed by keeping one face of the box always parallel and in contact with the table. The same procedure is repeated for four different faces.

Accelerometers:

as in Fig. 8-b, the box is placed on a table and smoothly (i.e. avoiding shocks) tilted by 90 deg along one edge, this is repeated four times¹ until the box returns in the initial position. The whole procedure is repeated with a different initial position.

Gyroscopes:

the procedure is similar to the one deployed for the accelerometers.

¹ Each time on a different edge: once a 90 deg rotation is performed along one edge, the next edge is the non-consecutive one which also makes contact with the table.

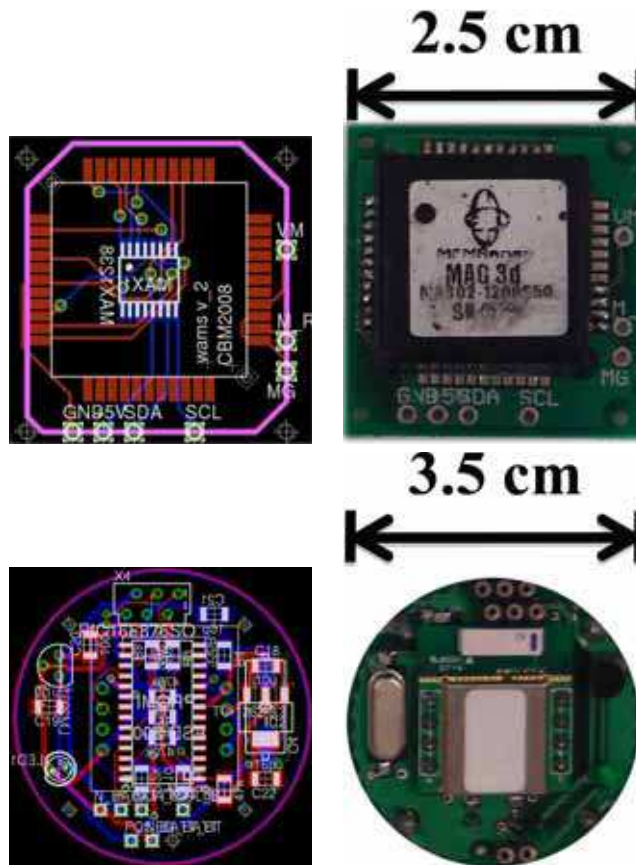


Fig. 6. The electronic CAD designs (left) and the real pictures (right) of the sensor (top) and the transmission (bottom) boards.

Measurements derived from a calibration sequence are shown in Fig. 8-c and Fig. 8-d, respectively for the magnetometers and for the accelerometers. The least-squares algorithm is then used to derive the best fitting ellipsoids (one for the magnetometers and one for the accelerometers) whose surfaces contain the two sets of measurements.

As previously mentioned, since the geomagnetic field is constant, its components in the moving frame are bound to lie on the calibrating ellipsoid, not only during the calibration sequences but for every possible movement. For this reason, also movements performed during the regular use of the toy, i.e. when the infants plays with it, can be used for updating the calibration parameters, or at least for an on-line check. Similar procedures apply to accelerometers, paying attention to consider only the quasi-static movements, i.e. when accelerations of the movement itself are negligible with respect to gravity. Details about 'in-use' calibration can be found in (Lotters et al. 1998).

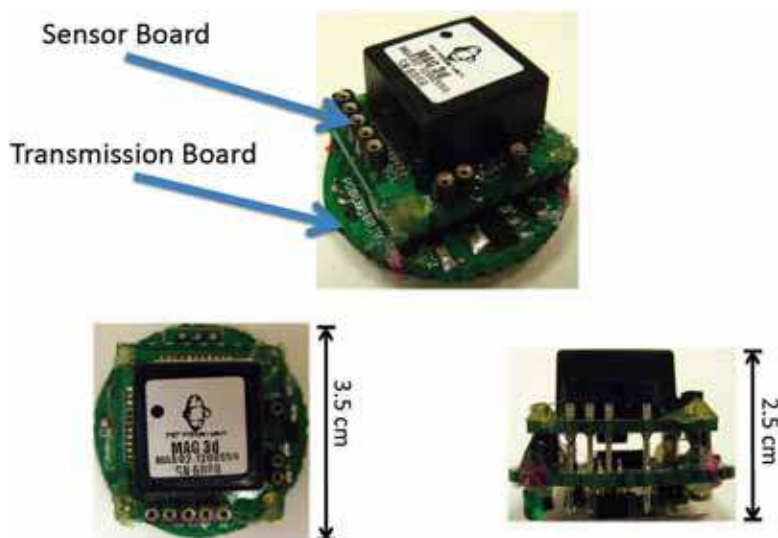


Fig. 7. Electronic core of the Block-Box platform with the actual dimensions.

3.2 Assessing Spontaneous Movements

Infants show a large variety of spontaneous movement patterns. Such movements are called spontaneous to tell them apart from reflex movements because they are endogenously generated by infants' nervous system without any external sensory input.

While reflexive movements allow a detailed study of a stable, quantitative relationship between sensory input and reflexive motor output, spontaneous motility could be regarded as the expression of spontaneous neural activity, so it is an excellent marker of neural dysfunction caused by brain impairments during the first year of life (Prechtl and General 2001).

Among several spontaneous motor patterns, movements that appear to be more effective for functional assessment of infants' nervous systems are complex sequential movements of arms, legs, neck, and trunk called General Movements (GMs): they are characterized by rotations along the axis of the limbs and slight changes in the direction of movements (see (Einspieler et al. 2005) for a review).

If the nervous system is impaired, GMs change their quality or even disappear: they lose their complex character and involve a reduced number of limbs in monotonous sequences; they appear to be rigid and less smooth because generated by the almost simultaneous contraction of all limb and trunk muscles. Such alterations are considered to be highly predictive for later neurological impairments like Cerebral Palsy (CP).

During the assessment phase, infants with bare arms and legs are videotaped in supine position. The duration of the recording depends on the age of the infant: to collect at least three GMs, 1 h recording is necessary with pre-term infants while 10 minutes are enough from term age onward. The same infant is videotaped at different ages: from 2 to 3 recordings during the pre-term period; one recording at term or early post-term age or both, and at least one recording between 9 and 15 weeks post-term. After each recording session, a trained clinician reviews the videotape looking for GMs sequences that are copied onto an assessment tape. The observed GM and the week of development are reported on a table called individual

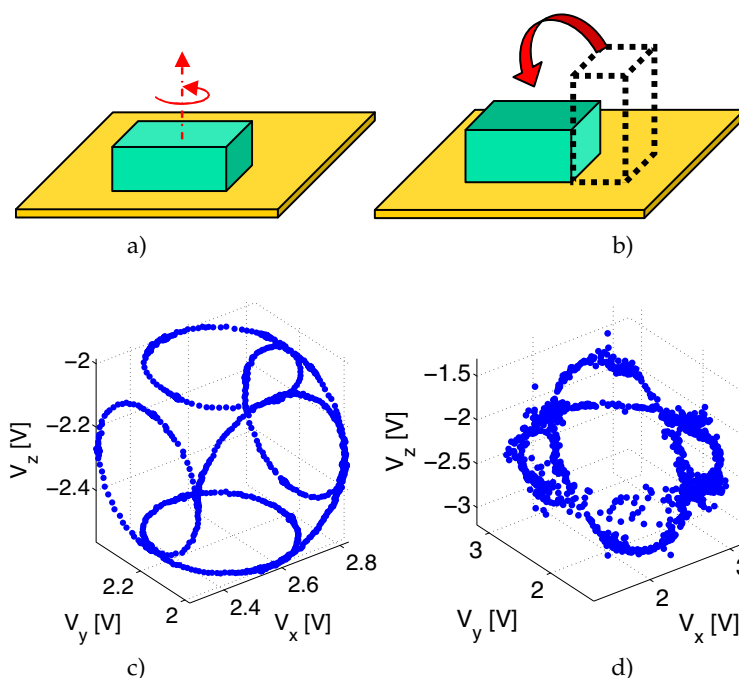


Fig. 8. Calibration sequences for magnetometers (a) and accelerometers (b). Plots of the measurements (i.e. voltages V_x , V_y and V_z from the triaxial sensors) derived from the calibration sequences for the magnetometers (c) and the accelerometers (d).

developmental trajectory. Such table is used to assess the risk of developing lateral neurological impairments. 11 studies on 358 infants assessed by 90 observers revealed an inter-rater reliability between 89% and 93% (Einspieler et al. 2005).

Wrist and Ankle Movement Sensor (WAMS)

GMs assessment protocol collects qualitative information on motor behavior of infants during their first year of life. In order to match the individual developmental trajectory with some quantitative objective information we proposed a magneto-inertial wearable device for ecological behavioral analysis of infants' motor behavior called Wrist and Ankle Movement Sensor (WAMS) (Taffoni et al. 2008). Such a device, which allows gathering objective information such as the angle of rotation along the axis of the limb, its velocity, smoothness, acceleration etc., could improve the predictive validity of GMs, thus reducing the inter-observer disagreement.

Because the target is assessing infants' movement, it is important to reduce size and weight of the device as much as possible. Although there are several commercial solutions, they are often exceedingly large and bulky. According to anthropometric data, the maximal linear length of a wearable device should not exceed 2.5 cm and should not weight more than 20 grams.

In order to estimate a proper scale range of the sensor, preliminary quantitative experiments have been conducted. A three-camera (500 Hz) motion capture system was used (Qualysis

Motion Capture Systems Inc., SWE) to obtain position-time data from both arms of infants and evaluate frequency and dynamic content of their spontaneous movements. Three reflective markers were placed on the head and two on both hands. In Fig. 9-A data from one-week-old infant are shown.

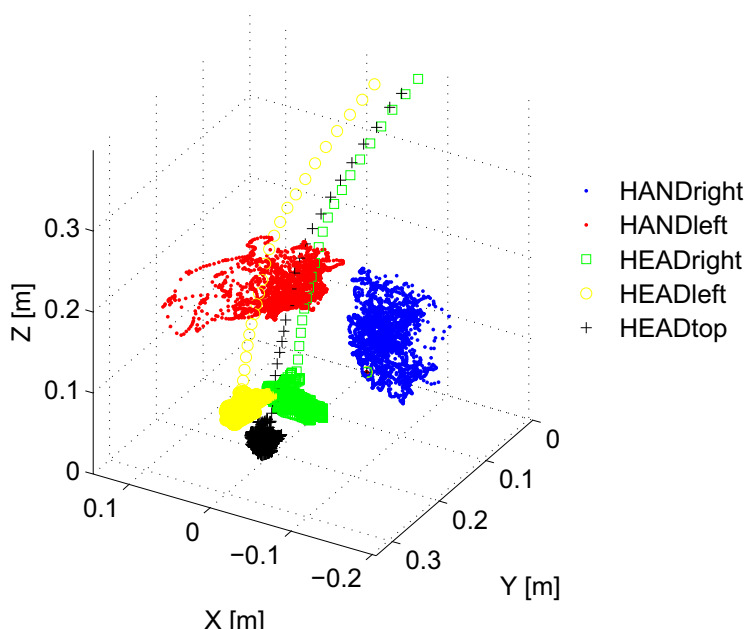


Fig. 9. Representative data relative to head-hands kinematics of a one week old infant

Probability Density Function (PDF) of several sets of experimental data was computed to estimate the dynamic range for the accelerometer sensors, showing that a $\pm 2g$ range would be sufficient to capture infants' kinematics. As for the magnetometers, since only the geomagnetic field (about 0.6 gauss) needs to be measured, the full measurement range should be in the order of ± 1 Gauss. Saturation of gyroscopes would result in a problematic loss of tracking and therefore, given several commercially available gyroscopes with full scale ranging from ± 150 deg/s to ± 1200 deg/s, the maximum scale range (± 1200 deg/s) was selected.

In line with such specification a sampling frequency of 250 Hz was selected. This frequency is between the sampling frequency of other magneto-inertial commercially available systems (typically 100 Hz) and the frequency of the optical devices (up to 500 Hz).

A preliminary analysis of commercial magneto-inertial sensors currently available highlighted a triaxial magnetometer, accelerometer and gyroscope analogue sensor from Mem-sense (MAG02-1200S050) that matches the technical requirements previously defined. Although there are several highly miniaturized components available off the shelf, we have chosen to use a microfabricated device integrating all the required sensing capability for two main reasons: 1) a more efficient packaging; 2) a more reliable axis orientation. Not orthogonal sensible axes directly translate in errors during orientation tracking. In order to simultaneously

collect data from both arms and legs we propose a Body Area Network (BAN) of four sensors: two for arms and two for legs. Unlike common BAN (Jovanov et al. 2005) we chose to use a wired configuration in order to reduce the weight of each sensor: wired communication allows not to include the battery onboard, and therefore to reduce the weight. For such reasons each sensing unit is provided with a low power, 12-channels, 12 bits AD Converters with an I2C compatible two wires serial interface. In this way only 4 wires are required: 2 for data and 2 for supply, which is in a remote master station. In this station a microcontroller PIC16F876A collects data from each WAMS (identified by a unique address) and retransmits via RS232 to a PC where such data are stored. The electronic board is embedded into a soft silicon rubber structure used both for electrical passivation and for comfortable contact with the infant's skin. A Velcro strap is used to fix such sensors to the infant's limbs. Figure 10 shows the first WAMS prototype: total weight less than 14 grams and volume within $2.5 \times 2.5 \times 1.5 \text{ cm}^3$.

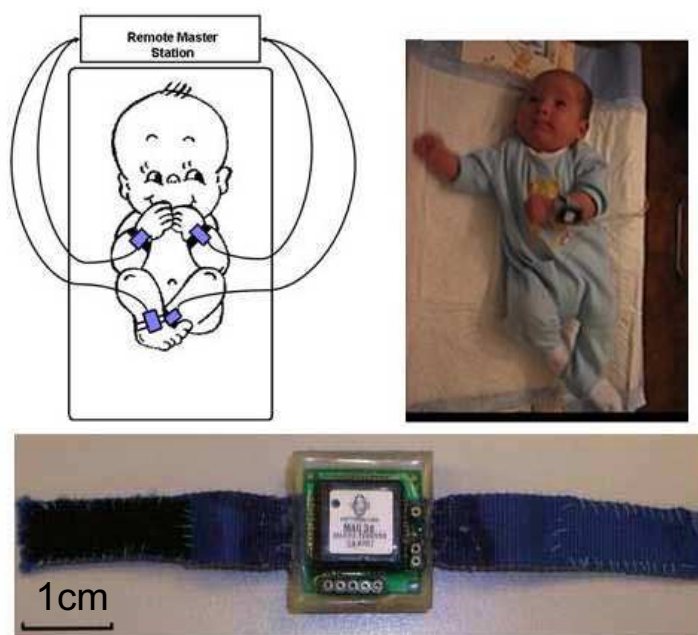


Fig. 10. Typical experimental scenario. (A). Example of use on a 3 months old baby (B). First WAMS prototype (C).

3.3 Assessing Social Attention

Poor sensorimotor integration has long been addressed as a cause of motor and social problems in developmental disorders such as ASD (Trevvarthen and Daniel 2005). Failure in orienting towards occurring social stimuli (e.g. facial expressions, speech, gesture) represents one of the earliest and most basic social impairments in autism and may contribute to the later-emerging social and communicative impairments (Dawson et al. 2004). Early social exchanges require rapid shifting of attention between different stimuli. Impairments in social orienting can alter the developmental pathway of young children by depriving them of appropriate social stimulation (Mundy and Neal 2001).

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