# Dynamic Space-Code Multiple Access (DSCMA) System: A Double Interference Cancellation Multiple Access Scheme in Wireless Communications System

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### 1. Introduction

It is well known that cellular mobile phone systems have evolved from 1G and 2G that use frequency and time division multiple access (FDMA and TDMA) systems respectively, to code division multiple access (CDMA) of third generation (3G) systems (Chen et al., 2006). Furthermore, the exploitation of spatial diversity from the emergence of advance antenna technologies such as smart antenna and space time signal processing have given rise to induce another multiple access scheme called space division multiple access (SDMA) systems (Fang, 2002). Among these schemes, the system capacity and spectrum efficiency are the key factors to compare the performances of various mobile communication systems.

Since radio frequency (RF) spectrum is a limited resource, these techniques have approached their fundamental limitations. Flexible utilization of such resources in space, time and code has led to great improvement in system capacity. For a given bandwidth, the system capacity for narrowband radio systems such as FDMA and TDMA is dimension or bandwidth limited. In contrast, the system capacity of CDMA and SDMA systems is interference limited. Any reduction in interference in CDMA and SDMA systems converts directly and linearly into increased capacity (Yu et al., 2004), (Chen et al., 2008).

Multiple access schemes such as FDMA and TDMA increase their system capacity and spectrum efficiency by dividing the different network planning phases more clearly into individual parts to allow different frequencies to be used at different time moments (Castaeda & Lara, 2008). In CDMA systems, the same frequency is used simultaneously in adjacent cells and the interference level should be taken into account in the coverage-planning phase (Niemela & Lempiainen, 2003). Furthermore, cell splitting and sectorisation to form SDMA systems with use of directional antenna could also result in increase of system capacity and spectrum efficiency over the omnidirectional antenna system (Godara,

1997). Although these approaches do significantly increase the system capacity and spectrum efficiency, each scheme basically is attempting a more efficient use of the same resource.

It is well known that CDMA system is characterized as being interference limited. Independent simultaneous transmissions by mobile users at different locations in a cell give rise to the near-far phenomenon. To combat the near-far problem, power control is used to ensure equal signal levels are received from all mobile users at different location (Hashem & Sousa, 1997). Therefore, power control is considered the most important system requirement for CDMA systems to increase the system capacity on the reverse link by overcoming the near-far problem (Cameron & Woerner, 1996), (Uthansakul, 2002). Since all the cells can operate with the same channel in CDMA cellular network, a significant source of interference apart from traffic in its own cell is the traffic from neighbouring cells. Thus, the system capacity of CDMA systems is determined by the amount of co-channel interference that it can tolerate, which is comprised of intra-cell interference and inter-cell interference (Wu et al., 1998). If the traffic load in neighbouring cells is reduced, more traffic can be accepted in the observed cell (Chatovich & Jabbari, 1999). However, because of power control from observed cell base station (BS), transmitting a high power level in reverse link may result in high interference to neighbouring cell BS (Hashem & Sousa, 1997). Therefore, in CDMA systems, if the capacity of a single cell increases it creates higher interference to its neighbouring cells and thus impacts their capacity.

Other approach that shows a promise for substantial capacity enhancement is the use of spatial filtering with exploitation of smart antenna at cell site BS (Zheng et al., 1996). Hence, the deployment of SDMA system has been recognised as one of the most promising techniques for controlling co-channel interference in cellular systems, leading to the required system capacity improvement (Liberti & Rappaport, 1998). The beamforming ability of smart antenna technology has been adapted to increase the gain of the desired signal while null interference sources resulting in the improvement of the system capacity (Huang et al., 2001). The narrow beams from smart antenna are steered toward desired users in order to filter out interference caused by co-channel users located in the same cell and from adjacent cells (Galvan-Tejada & Gardiner, 2001).

However, in order to achieve an ideal SDMA system, smart antenna must carefully form its radiation patterns to capture the desired user and to nullify sufficiently interfering users. Therefore, the smart antenna requires high accuracy in propagation channel response estimation (Cho et al., 2002). If there are N elements antenna array used in a smart antenna system, it is only possible to accommodate N - 1 users in reverse link (Rapajic, 1998), (Kim et al., 2001). Actually in the randomness of mobile users distribution, this is not always possible to eliminate interferers by null-steering in the corresponding arrival directions. Hence, there will be a probability of two or more mobile users located near to each other. This means that the co-channel interferences will occur among these mobile users when adaptive beams steering smart antenna are employed. On the other hand, the present of sidelobes from smart antenna system will further reduce the signal to interference ratio (SIR) performance of each mobile user. Hence, more sidelobes interferences are radiated in the direction of the desired user main lobe pattern. These sidelobes interferences can significantly reduce the system capacity if multiple beams are synthesized from smart antenna to accommodate the density of mobile users in a particular area.

The wireless channel usually characterized by the path loss, shadowing and fading (Feuerstein et al., 1994). In urban areas, multipath propagation is common, whereby the receiver observes a number of copies of the transmitted signal, each with a different time delay (Adachi et al., 2005). This provides a form of multipath fading. In a digital communication system, the delay-spread of multipath propagation could also cause intersymbol interference (ISI) (Lien & Cherniakov, 1998). The characteristics of the spreading sequences in CDMA system provide a crucial effect on the performance of the whole communication systems. This signature sequences in general determine how much interference is received at a receiver from other mobile users and influence the extraction capability of the desired signal from noise-like spectrum (Xie & Rahardja, 2005). On the other hand, since the reverse link of a CDMA system is usually asynchronous, in the sense that the arrival times for each mobile user signal are different (Thompson et al., 1996), (Choi et al., 2007). Therefore, the spreading sequences of CDMA systems are characterized with ISI as well as multiple access interference (MAI) (Peterson et al., 1995), (Guo & Wang, 2008). In multipath propagation environment, multiple copies of transmitted signal arrive at receiver with different time delay will cause ISI. A MAI occurs if the orthogonality among spreading sequences is lost (Ishida et al., 2000). The MAI is caused by asynchronous in a CDMA system where each mobile user will observe interference from all other mobile users in the system, since the transmitted signal will not be orthogonal in delay-spread environment (Thompson et al., 1996). Traditional CDMA spreading sequences such as m-sequence (Golomb, 1992), Gold codes (Gold, 1967), and Kasami codes (Kasami, 1966), exhibit non-zero cross-correlation which results in high MAI in asynchronous reverse link transmission. Another family of orthogonal codes is constituted by Walsh codes (Harmuth, 1970) and orthogonal Gold codes (Popovic, 1997), do retain their orthogonality in the case of perfect synchronization, but also exhibit non-zero cross-correlation in asynchronous transmission (Wei et al., 2005). Recently, an attractive family of large area synchronized (LAS) CDMA spreading sequences is introduced in (Li, 2003) has exhibited zero correlation zone (ZCZ) or interference free window (IFW) near zero delay time offset, resulting in zero ISI and MAI within the IFW. The LAS spreading sequence is constituted by the combination of Large Area (LA) code (Li, 1999) and Loosely Synchronous (LS) code (Staňczak et al., 2001). More specifically, the interference-free in CDMA system only become possible when the maximum channel-induced delay-spread is within the designed IFW duration. However, in the system design especially using omnidirectional antenna, not all multipath signal components arrive within IFW time offset. Since the total duration of IFW expressed in terms of the number of chip intervals depend on the minimum zero padding implanted between non-zero pulses interval, thus the number of minimum zero padding must be increased to maximum delay-spread of the channel in LAS sequence in order to accommodate all multipath signal components. This implies that the duty ratio of LAS spreading sequences is low when the number of minimum zero padding is increased. Therefore, a specific drawback of LAS-CDMA is that its relatively efficient orthogonal codes demanded in wireless systems are limited, and hence reduce its spectrum efficiency. Besides that, the implementation of LAS sequences is very complex that additional components are necessary.

There have been many multiple access systems for the cellular system designed to improve its system performance. Several works have been carried out to show the improvement in the system capacity using the joint multiple access system. A careful selection of joints multiple access from two or more individual systems can determine the fitness of the joint system. Interference-limited systems such as CDMA and SDMA are susceptible to time of arrival (TOA) and angle of arrival (AOA) of individual user signals. Thus, a non-uniform traffic can severely degrade the performance of CDMA and SDMA systems. In this chapter, a joint multiple access of CDMA and SDMA system is proposed. The performance of this joint multiple access system is also vulnerable to the non-uniform traffic. Although the performance of this joint multiple access system has been previously studied in several papers (Liberti & Rappaport, 1994), (Naquib et al., 1994), (Buracchini et al., 1996) and (Ng & Sousa, 1998), none of them considers to evaluate the most realistic of system performance in this joint multiple access.

In this chapter, a new approach called dynamic space-code multiple access (DSCMA) system arising from the combination of CDMA and SDMA systems is designed, and its system performances are then investigated. An innovative approach to eliminate the existing interferences in DSCMA system is introduced. The spreading sequences of Large Area Synchronous Even Ternary (LAS-ET), which exhibited an interference free window (IFW) in their correlation, are exploited here. The spatial signature from smart antenna narrower beam is exploited to drive all the multipath propagation signals to arrive within the IFW in reverse link transmission. The size of IFW is adaptable with the size of smart antenna beamwidth through dynamic space-code (DSC) algorithm. Therefore, the result of combined dominant signature from DSCMA system will yield a perfect interference cancellation so that the system capacity increases dramatically.

#### 2. The Properties of Orthogonal CDMA Sequences

Traditional ways of separating multiple access signals in time or frequency such as TDMA and FDMA are relatively simple by making sure that the signals are orthogonal and non-interfering. However, in CDMA different mobile users occupy the same bandwidth at the same time. They are separated from each other through the use of a set of orthogonal sequences. Two waveforms *x* and *y* are said to be orthogonal to each other if their cross-correlation,  $R_{xy}(0)$  over *T* period is zero in time shift  $\tau$  (Lee, 1998), where

$$R_{xy}(\tau) = \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} x(t) y(t+\tau) dt$$
(1)

In discrete time, the two sequences *x* and *y* are orthogonal if their cross product  $R_{xy}(0)$  over *T* period is zero (Wang et al., 2007). The cross product of  $R_{xy}(\tau)$  is defined as

$$R_{xy}(\tau) = \sum_{\tau=-T}^{T} x(t) y(t+\tau)$$
<sup>(2)</sup>

As an example, the following two sequences or codes, *x* and *y* are orthogonal.

$$x = \begin{bmatrix} -1, -1, +1, +1 \end{bmatrix}$$
(3)

$$y = [-1, +1, +1, -1] \tag{4}$$

Hence, their cross-correlation is zero.

$$R_{xy}(0) = (-1)(-1) + (-1)(+1) + (+1)(+1) + (+1)(-1) = 0$$
(5)

In order for the set of codes to be used in a multiple access scheme, an additional property is needed. In addition to the zero cross-correlation property, each code in the set of orthogonal codes must have an equal number of +1s and -1s (Faruque, 1996). This second property gives that particular code the pseudorandom nature. A direct sequence CDMA (DS-CDMA) system spread the baseband data by directly multiplying the baseband data pulses with a peudorandom or PN sequence that is produced by a PN code generator. A single pulse or symbol of the PN waveform is called a chip, where the chip rate is much higher than the data bit rate (Lee, 1991).

#### 2.1 Welch Bound in CDMA Systems

The CDMA system is a multiple access scheme in which several independent users access a common communication channel by modulating their data symbols with preassigned spreading sequences. The receiver observes the sum of the transmitted signals in additive white Gaussian noise (AWGN) channel. The decoder for a given mobile user treats the sum of the interfering signals from other mobile users as noise. The spreading sequences are chosen to create good single user channels for the individual coding systems. In fact, however, the channel created by the spreading sequences is susceptible to MAI (Rupf & Massey, 1994). In 1974, Welch in (Welch, 1974) had shown that the lower bound for the

acceptable sidelobes of auto-correlation and cross-correlation functions are set around  $SF^{-\frac{1}{2}}$ , where *SF* is the spreading factor or processing gain of the system. This lower bound is called as Welch bound (Li, 2003). Signature sequences that maximize the sum capacity in the uplink of CDMA systems in AWGN channel are known to satisfy Welch's bound on the total squared correlation with equality (Heath et al., 2004).

#### 2.2 LAS-ET Sequences

The original LAS codes proposed in (Li, 1999) are synthesized by seeding LS codes in LA codes to improve it spectrum efficiency. An  $N_p$  LA codes are synthesized in such a manner that the  $N_p$  non-zero ±1 pulses from *m*-sequences oriented are positioned as shown in Table 1. This arrangement forms a configuration of  $LA(N_p, K_0, L_c)$  where  $K_0$  is the minimum number of zero padding in pulse interval of non-zero pulses which determine the size of IFW delay-spread in term of chips, while having a total code length of  $L_c$  chips.

	0	38	78	120	164	210	258	308	360	414	470	530	592	660	732	808	847
C1	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
C2	+	+	+	+	-	-	-	-	+	-	+	-	-	+	+	-	+
C3	+	+	+	-	-	-	-	+	-	+	-	-	+	+	-	+	+
C4	+	+	-	-	-	-	+	-	+	-	-	+	+	-	+	+	+
C5	+	-	-	-	-	+	-	+	-	-	+	+	-	+	+	+	+
C6	+	-	-	-	+	-	+	-	-	+	+	-	+	+	+	-	+
C7	+	-	-	+	-	+	-	-	+	+	-	+	+	+	-	-	+
C8	+	-	+	-	+	-	-	+	+	-	+	+	+	-	-	-	+
C9	+	+	-	+	-	-	+	+	-	+	+	+	-	-	-	-	+
C10	+	-	+	-	-	+	+	-	+	+	+	1	-	-	-	+	+
C11	+	+	-	-	+	+	-	+	+	+	-	-	-	-	+	-	+
C12	+	-	-	+	+	-	+	+	+	-	-	I	-	+	1	+	+
C13	+	-	+	+	-	+	+	+	-	-	-	-	+	-	+	-	+
C14	+	+	+	-	+	+	+	-	-	-	-	+	-	+	-	-	+
C15	+	+	-	+	+	+	-	-	-	-	+	-	+	-	-	+	+
C16	+	-	+	+	+	-	-	-	-	+	-	+	-	-	+	+	+

Table 1. The arrangement of 16 LA(16,38,847) sequences

In order to exploit the characteristics of LA sequences proposed in (Li, 1999) without altering the size of its IFW, a modified version of the sequence such LAS-ET sequences (Ng et al., 2009) is employed in DSCMA instead of LAS-CDMA sequences proposed in (Li, 2003) which exhibit a small IFW. Figure 1 shows the correlation properties of the LAS - ET(16,38,818) sequences. As can be seen in these figures, the correlation properties of LAS - ET(16,38,818) sequences are similar to the original proposed LA(16,38,847) sequences which exhibited a large IFW around the origin. The cross-correlation value of LAS - ET(16,38,818) sequence in zero delay spread is  $4.03 \times 10^{-17}$ .





Fig. 1. Correlation properties of LAS - ET(16,38,818) sequence; (a) auto-correlation and (b) cross-correlation.

#### 3. Reverse Link Capacity of SDMA System

The conventional SDMA systems increase its capacity by spatial filtering the interferences. The system continuously adapts its narrower beam from smart antenna system to steer each mobile user with the main lobe while isolating interferences with nulls. Hence, SDMA is allowed to reuse the limited radio resources (frequency, time and code) within a cell. From Equation (1) in (Ng et al., 2008), the nulls' AOA,  $\psi_{nulls}$  of the SDMA radiation pattern occur at

$$\psi_{nulls} = \cos^{-1} \left[ 2 \left( \frac{h}{N_e} - \frac{\alpha}{2\pi} \right) \right]$$
(6)

where  $N_e$  is the number of elements in smart antenna system,  $\alpha$  is progressively phase shift, and *h* is any integer but not equal to 0, *n*, 2*n*, .....

Figures 2a and 2b show the typical SDMA system for  $N_e = 8$  and 32 respectively with 90° AOA of the desired user. For  $N_e = 8$ , the nulls to accommodate interfering users are occurred at 41.41°, 60°, 75.52°, 104.48°, 120° and 138.59°, while the nulls for  $N_e = 32$  are occurred at 20.36°, 28.96°, 35.66°, 41.41°, 46.57°, 51.32°, 55.77°, 60°, 64.06°, 67.98°, 71.79°, 75.52°, 79.19°, 82.82°, 86.42°, 90°, 93.58°, 97.18°, 100.81°, 104.48°, 108.21°, 112.02°, 115.94°, 120°,

124.23°, 128.68°, 133.43°, 138.59°, 144.34°, 151.05° and 159.64°. These figures show that the system capacity, *K* of SDMA system is direct proportional to the number of antenna elements in smart antenna with expression below (Rapajic, 1998)

$$K = N_e - 1 \tag{7}$$

The interfering users are only allowed to be located at null AOAs, otherwise co-channel interferences between mobile users will occur. Any additional mobile user into this system after the limited nulls are fully occupied will also cause co-channel interference to other mobile users.



Fig. 2. Radiation pattern of SDMA system for (a)  $N_e = 8$  and (b)  $N_e = 32$ .

It has been reported that smart antenna can synthesize a high directive beam toward the desired user while nulling the interfering users to increase capacity. However, fully nulling the interfering users in SDMA system do not take place because there are two major interference sources, which are side-lobes and co-channel interferences. The interfering users will not always locate at the nulls of the desired user radiation pattern especially in randomly distributed traffic environment as shown in Figure 3.



Fig. 3. Co-channel and side-lobes interferences to the desired user, C from randomly located interfering users of 1, 2, 3, 4,...., 16

## 4. Dynamic Space Code Multiple Access (DSCMA) System

Non-uniformly distributed traffic usually degrades the performance of CDMA and SDMA systems severely in the reverse link. The imperfect correlation properties of the traditional CDMA spreading sequences result in ISI and MAI at non-zero delay spread. The random positions of mobile users will cause MAI among them in the SDMA system, where positions at nulls of the desired user radiation pattern are rarely achieved. Therefore, the non-uniform traffic causes loss of orthogonality to distinguish each mobile user in the conventional interference limited systems.

Here, a promising solution to deploy the BS with smart antenna system to perform the joint multiple access of CDMA and SDMA systems is proposed. The CDMA and SDMA systems are adapted to each other dynamically to form DSCMA system. This proposed multiple access scheme is a novel interference cancellation scheme that employ the spreading sequences of CDMA system into spatial signatures of SDMA system through DSC algorithm. In DSC algorithm, the size of dedicated IFW from LAS-ET spread sequence is

adapted dynamically to the size of half power synthesized beamwidth from smart antenna beamforming system as shown in Figure 4. In this joint multiple access scheme, each user is assigned an LAS-ET sequence within a high directivity beam. Hence, the integration of these two signature schemes, spatial filtering and spreading sequence, creates a dominant signature scheme called DSC signature. Therefore, by using this dominant signature scheme, the inherent interferences in CDMA and SDMA systems environment can be eliminated.



Fig. 4. Performance of various beamwidths in smart antenna system over IFW region from correlation property of LAS - ET(16,38,818) sequences.

As shown in previous section, the co-channel interference between two mobile users in SDMA system occurs when both of them are located close to each other. For example, assuming that the desired user, *C* is located at AOA of 90° to the smart antenna axis while other mobile users are randomly located within the AOA of 0° to 180° as shown in Figure 3. It is observed that the 11<sup>th</sup> user's beam is located very near to *C* with only 0.6° separation. This phenomenon causes co-channel interference between them while other mobile users also contribute interferences to *C* through their sidelobes radiation pattern. It is possible to mitigate these co-channel interferences by CDMA spreading sequences. However, all traditional CDMA spreading sequences are self-interference systems when all signals from each mobile user arrive at the BS in asynchronous manner. The auto-correlation and cross-correlation properties of traditional CDMA sequences are not orthogonal at non-zero delay

spread,  $\tau > 0$ . Thus, it shows that interference occur among the mobile users in asynchronous transmission environment.

Therefore, it is necessary to prefer spreading sequences that exhibit zero correlation between each other to drive all the asynchronous signal components to drop within the smart antenna's narrow beam maximum propagation delay spread. Hence, a spreading sequence that exhibits large size of IFW is required to accommodate large beamwidth of smart antenna radiation pattern. Considering Figure 3 again, there is group of beams with theirs AOA respectively to accommodate 17 randomly distributed mobile users. Each beam is assigned to different mobile user with an LAS sequence order, C1, C2, C3, C4, C5,..., Cm, where m is the maximum number of total available sequence. These sequences are assigned to mobile users in chronological order upon their arrival and can be reused dynamically whenever needed.

To illustrate how directive beam can improve the reverse link in a single cell of DSCMA system, consider the case in which each mobile user has an omnidirectional antenna, and the BS tracks each mobile user in the cell using a directive beam. Assume that the beam pattern,  $G(\psi)$  in formed such that the pattern has a maximum gain in the AOA of the desired user. Such a directive pattern can be formed using an  $N_e$  elements smart antenna array. Assume that *K* users in the single cell of DSCMA system are non-uniformly distributed throughout a cell. On the reverse link, the power received from the desired user signal is  $P_{r,0}$  with maximum gain of  $G_0(\psi_0)$ . The received powers from K - 1 interfering users are given by  $P_{r,i}$  for  $i = 1, 2, \dots, K - 1$ . Then the average total received interference power, *I* seen at the desired user AOA,  $\psi_0$  at the BS is given by

$$I = E\left\{\sum_{i=1}^{K-1} G_i(\psi_0) P_{r,i}\right\}$$
(8)

where  $G_i(\psi_0)$  is the *i*th interference gain level of smart antenna radiation pattern seen at the AOA of the desired user. The value of  $G_i(\psi_0)$  can be obtained from Equation (1) in (Ng et al., 2008) and is given as

$$G_i(\psi_0) = \frac{1}{N_e} \left| \frac{\sin N_e(\pi k \cos \psi_0 + \alpha_i/2)}{\sin(\pi k \cos \psi_0 + \alpha_i/2)} \right|$$
(9)

where *k* is given as 0.5 for half wavelength spacing between elements to avoid the appearance of grating lobe in the system, and parameter  $\alpha_i$  is the phase shift of the smart antenna to steer the beam in  $\psi_i$  direction of *i*th interfering user. If the perfect power control is applied such that the received power at the BS antenna from each mobile user is the same, then  $P_{r,i} = P_c$  for each of *K* users, and hence the average interference power seen by the desired user is given by

$$I = P_c E\left\{\sum_{i=1}^{K-1} G_i(\psi_0)\right\}$$
(10)

#### 5. Reverse Link Interferences in DSCMA System

In DSCMA system, a BS equipped with smart antenna transmits signal to each mobile user in forward link transmission using a synthesized narrow beam and a dedicated spreading sequence. The signal is perfectly synchronized at transmission so that it arrives at mobile receiver in synchronism with zero delay spread. Consequently, due to the orthogonalities of both spatial signature and spreading sequence in zero delay spread among the *K* users in a cell, each mobile receiver can demodulate its own signal without interference from other transmitted signals that share the same channel.

However, this synchronism in forward link transmission cannot be maintained in reverse link transmission where all the signals from K users are rather arrived at BS in asynchronized manner. Thus, the signals from the other mobile users appear as additive interference to the desired user signal if the orthogonalities of both spatial signature and spreading sequence among them are loss in non-zero delay-spread. The reverse link interferences are twofold: the interference arising from K - 1 users in the same cell or can be known as intra-cell interference, and the interference arising from mobile users in neighbouring cells or also called as inter-cell interference. Hence, the system capacity of DSCMA is examined by considering both intra-cell and inter-cell interference environments in reverse link transmission.

#### 5.1 Intra-cell Interference

Suppose that each cell has *K* randomly distributed mobile users. With the use of perfect instantaneous power control, all *K* user signals are arriving at the BS with the same power level *S* within the same cell. Therefore, the intra-cell interference,  $I_{intra}$  from *K* – 1 interfering users is given as

$$I_{intra} = (K-1)S \tag{11}$$

In DSCMA system, the K - 1 interferences power level are not same in the AOA of the desired user,  $\psi_0$ . Nevertheless, the interfering signals from K - 1 users are still received at the same power level *S* from theirs respective AOA through perfect power control. Most of these interfering signals contribute merely side-lobe interferences with  $G_i(\psi_0) < S$  in  $\psi_0$  direction. Some of the interfering signals are also received at the same power level,  $G_i(\psi_0) = S$  when they are at the same AOA of the desired user.

The arbitrarily interferences level,  $G_i(\psi_0)$  as shown in Figure 3 with 16 interfering users can be analogously as multiple dots along the line of radiation pattern as shown in Figure 5. This is assuming that all radiation patterns for all mobile users are same. Hence, from (9) and (11), the intra-cell interference in AOA of mobile user *C*,  $I_{intra}(\psi_0)$  yields to

$$I_{intra}(\psi_0) = S \cdot \sum_{i=1}^{K-1} G_i(\psi_0) = \frac{S}{N} \cdot \sum_{i=1}^{K-1} \left| \frac{\sin N(\pi k \cos(\psi_0) + \alpha_i / 2)}{\sin(\pi k \cos(\psi_0) + \alpha_i / 2)} \right|$$
(12)



Fig. 5. The analogously random side-lobes interferences from 16 interfering users in AOA of the desired user

#### 5.2 Inter-cell Interference

In the multi-cell of DSCMA system, the interference analysis in reverse link becomes complicated. This is because the mobile users are power controlled by their own cell BS. The membership of the user is determined by the maximum pilot signal power among the cells and not the minimum distance from a cell BS. The mobile users are connected to a BS that offers the lowest signal attenuation rather than the closest BS (Gilhousen et al., 1991). Because of power control, the interference level received from mobile users in neighbouring cells depends on two factors: attenuation in the path to the desired user's cell BS, and attenuation in the path to the mobile user's cell BS. Thus, in the fourth power law of distance, the user's transmitted power  $P_t$  can be expressed as (Chatovich & Jabbari, 1999)

$$P_t = P_r r^4 10^{(\zeta/10)} \tag{13}$$

where  $P_r$  is the received signal power at its BS,  $\zeta$  is the log-normal Gaussian random variable with zero mean and standard deviation,  $\sigma$  of 8 dB, and *r* is the distance from the mobile user to BS. Since only average power levels are considered, the effects of multipath fading are ignored. To evaluate inter-cell interference,  $I_{inter}(\psi_0)$  in DSCMA, consider an

interfering user located in *m*th neighbouring cell at a distance  $r_m$  from its base station  $BS_m$  and  $r_0$  from the desired user base station  $BS_0$  as shown in Figure 6.



Fig. 6. Inter-cell interference environment model.

If  $P_t$  is its transmit power, the received power S at its BS is given by

$$S = \frac{P_t G_m(\psi_m)}{10^{(\zeta_m/10)} r_m^4}$$
(14)

where  $G_m(\psi_m)$  is the antenna gain in the AOA of the interfering user to its cell  $BS_m$ , and  $\zeta_m$  is the Gaussian random variable representing the shadowing process in its cell. Then the interference *I* received at  $BS_0$  is given by

$$I = \frac{P_t G_0(\psi_{mi})}{10^{(\zeta_0/10)} r_0^4}$$
(15)

where  $G_0(\psi_{mi})$  is the antenna gain of  $BS_0$  in the AOA of the *i*th interfering user from *m*th neighbouring cell to  $BS_0$ , and  $\zeta_0$  is the Gaussian random variable representing the shadowing process in the desired user cell.

Hence, from (14) and (15), the interference to signal ratio, I/S is given by

$$\frac{I}{S} = \left(\frac{r_m}{r_0}\right)^4 \cdot \left(\frac{G_0(\psi_{mi})}{G_m(\psi_m)}\right) \cdot 10^{(\zeta_m - \zeta_0)/10}$$
(16)

where the first term is due to the attenuation caused by distance and blockage to the given BS, while the third term is the effect of power control to compensate for the corresponding attenuation to its BS. Since  $\zeta_m$  and  $\zeta_0$  are independent their difference has zero mean and variance  $2\sigma^2$  (Cooper & Nettleton, 1978). The second term reveals the total antenna gain received in the AOA of the interfering user to the  $BS_{0r}$  and its value is less than unity. In DSCMA, this second term will only has a maximum value when an interfering user from a neighbouring cell is located at the same AOA of the desired user,  $\psi_0$ . Then  $G_0(\psi_{mi})$  in (16) will become

$$G_{0}(\psi_{mi}) = \frac{1}{N_{e}} \cdot \sum_{m=1}^{6} \sum_{i=1}^{K-1} \left| \frac{\sin N_{e}(\pi k \cos(\psi_{mi}) + \alpha_{0}/2)}{\sin(\pi k \cos(\psi_{mi}) + \alpha_{0}/2)} \right|$$
(17)

For all values of the parameters in (16), I/S is less than unity. If its value is not less than unity then the user would switch to the other cell BS. Therefore,  $I_{inter}(\psi_0)$  in DSCMA is found by summing (16) for all mobile users in the first tier neighbouring cells

$$I_{\text{int}er}(\psi_{mi}) = \sum_{m=1}^{6} \sum_{i=1}^{K-1} S \cdot \left(\frac{r_{mi}}{r_{0i}}\right)^4 \cdot \left(\frac{G_0(\psi_{mi})}{G_m(\psi_m)}\right) \cdot 10^{(\zeta_{mi} - \zeta_{0i})/10}$$
(18)

where  $G_m(\psi_m) = 1$  which the gain to theirs mobile user is 1.

### 6. DSCMA System Signalling

To simplify the derivation, only the baseband signal of transmitted signal is being considered. Hence, in DSCMA system, the transmitted signal from the *i*th user,  $s_i(t)$  that occupies the *i*th spreading sequence for i = 1, 2, ..., K - 1 can be written as

$$s_i(t) = \sqrt{P}d_i(t)c_i(t) \qquad \qquad 0 \le t \le T$$
(19)

Assuming that the desired user is user 0 and all the other K - 1 users are interfering users. The received signal, r(t) is a sum of the transmitted signals from all K users and corrupted by its additive complex Gaussian thermal noise, n(t) in an AWGN channel. The signal of each mobile user arrives at a different propagation delay,  $\tau_i$ . Thus, the received signal at the BS equipped with smart antenna beamforming network in the AOA of user 0 can be expressed as

$$r(\psi_0, t) = \sum_{i=0}^{K-1} s_i (t - \tau_i) \sqrt{G_i(\psi_0)} + n(t) = \sum_{i=0}^{K-1} \sqrt{P} \sqrt{G_i(\psi_0)} d_i (t - \tau_i) c_i (t - \tau_i) + n(t)$$
(20)

where  $G_i(\psi_0)$  denotes as *i*th radiation pattern gain of *i*th user in the AOA of user 0. This equation signifies the combination of CDMA and SDMA by the terms  $G_i(\psi_0)$ . When

 $G_0(\psi_0)$  is normalized to 1, the generated  $G_i(\psi_0)$  will be less than 1 if the *i*th interfering user is not located at the same AOA as user 0. For a conventional CDMA system,  $G_i(\psi_0)$  will take the value of 1. This signal is then despread with the spreading sequence of user 0 at the receiver. A correlation-based detector is used to obtain the appropriate decision,  $z_0$  which can be derived as

$$z_{0} = \int_{0}^{T} r(\psi_{0}, t) c_{0}(t - \tau_{0} - \tau_{e}) dt$$
(21)

where  $\tau_e$  is the sequence synchronization error, which degrades the auto-correlation properties. If prefect synchronization is assumed as in the case of directional antenna, where the multipath fading effect is neglected, then  $\tau_0 = \tau_e = 0$ . Thus, Equation (21) leads to

$$z_{0} = \int_{0}^{T} r(\psi_{0}, t)c_{0}(t)dt$$

$$= \int_{0}^{T} \left[ \sqrt{P}\sqrt{G_{0}(\psi_{0})}d_{0}(t)c_{0}^{2}(t) + \sum_{i=1}^{K-1}\sqrt{P}\sqrt{G_{i}(\psi_{0})}d_{i}(t-\tau_{i})c_{i}(t-\tau_{i})c_{0}(t) \right] dt \qquad (22)$$

$$= S + I + \eta$$

#### 7. Probability of Error Evaluation in DSCMA System over AWGN Channel

A bit error rate (BER) expression for DSCMA is derived over MAI from the other K – 1 users in an AWGN channel. The derivation is performed at the baseband level, which will simplify the analysis. From the previous section, the first term of (22), *S* is the transmitted signal of user 0, where

$$S = \int_{0}^{T} \sqrt{P} \sqrt{G_{0}(\psi_{0})} d_{0}(t) c_{0}^{2}(t) dt$$
(23)

Considering that  $G_0(\psi_0) = 1$ ,  $c_0^2(t) = 1$  and  $d_0 = \pm 1$ , thus Equation (23) becomes

$$S = \pm \sqrt{PT} \tag{24}$$

The term  $\eta$  in (22) is the noise component due to n(t) in AWGN channel, which corresponds to the despread term of n(t) attributes to

$$\eta = \int_0^T n(t)c_0(t)dt \tag{25}$$

Since n(t) is the zero mean AWGN having a variance of  $\sigma^2 = N_0/2$ , thus  $\eta$  is also a zero mean Gaussian variable and a variance of  $Var[\eta]$ , which is derived as

$$Var[\eta] = E[\eta^{2}]$$

$$= E\left[\int_{0}^{T} n(t)c_{0}(t)dt\int_{0}^{T} n(u)c_{0}(u)du\right]$$

$$= \int_{0}^{T}\int_{0}^{T} E[n(t)n(u)]c_{0}(t)c_{0}(u)dtdu$$
(26)

But E[n(t)n(u)] is the auto-correlation of n(t), where

$$E[n(t)n(u)] = \frac{N_0}{2}\delta(t-u)$$
(27)

Therefore, the variance of (26) becomes

$$Var[\eta] = \frac{N_0}{2} \int_0^T \int_0^T \delta(t-u) c_0(t) c_0(u) dt du$$
  
=  $\frac{N_0}{2} \int_0^T c_0^2(u) du$   
=  $\frac{N_0 T}{2}$  (28)

The term *I* in (22) is the MAI component of the *K* – 1 interferers, which is given by

$$I = \sum_{i=1}^{K-1} \sqrt{P} \sqrt{G_i(\psi_0)} \int_0^T d_i (t - \tau_i) c_i (t - \tau_i) c_0(t) dt$$
(29)

Since  $\int_{0}^{T} c_{i}(t-\tau_{i})c_{0}(t)dt$  is cross-correlation between sequences  $c_{i}$  and  $c_{0}$ , thus

$$\int_{0}^{T} c_{i}(t-\tau_{i})c_{0}(t)dt = R_{i,0}T$$
(30)

and  $d_i(t - \tau_i) = \pm 1$ , therefore *I* is reduced to

$$I = \pm \sqrt{PT} \sum_{i=1}^{K-1} \sqrt{G_i(\psi_0)} R_{i,0}$$
(31)

The signal to interference plus noise ratio (SINR) is then given as

$$SINR = \frac{S^2}{Var[\eta] + I^2}$$
(32)

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